On-sky multiwavelength phasing of segmented telescopes with the Zernike phase contrast sensor

Arthur Vigan,1,2,* Kjetil Dohlen,1 and Silvio Mazzanti1

1Laboratoire d’Astrophysique de Marseille, UMR 6110, CNRS, Université de Provence, 38 rue Frédéric Joliot-Curie, 13388 Marseille Cedex 13, France
2Astrophysics Group, School of Physics, University Of Exeter, Stocker Road, Exeter EX4 4QL, United Kingdom

*Corresponding author: arthur@astro.ex.ac.uk

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Future extremely large telescopes will adopt segmented primary mirrors with several hundreds of segments. Cophasing of the segments together is essential to reach high wavefront quality. The phasing sensor must be able to maintain very high phasing accuracy during the observations, while being able to phase segments dephased by several micrometers. The Zernike phase contrast sensor has been demonstrated on-sky at the Very Large Telescope. We present the multiwavelength scheme that has been implemented to extend the capture range from $\lambda/2$ on the wavefront to many micrometers, demonstrating that it is successful at phasing mirrors with piston errors up to $4 \mu m$ on the wavefront. We discuss the results at different levels and conclude with a phasing strategy for a future extremely large telescope. © 2011 Optical Society of America

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1. Introduction

Large telescopes have always been an important driver for astrophysical discoveries, leading to the design and construction of several 8 to 10 m telescopes. Practical aspects related to manufacturing and handling limit the size of monolithic mirrors to ~8 m, forcing the adoption of segmented primary mirrors to reach larger diameters, e.g., for the Keck telescopes and the Gran Telescopio Canarias. Both of them are constituted of 36 hexagonal segments of ~0.9 m each, resulting in a total diameter of 10 m. The next generation of extremely large telescopes (ELTs), which is currently being designed, will naturally adopt segmented primary mirrors to reach diameters from 30 to 42 m. The two main telescopes of the ELT era will be the thirty meter telescope [1], 30 m in diameter with 492 segments, and the European ELT (E-ELT) [2], 42 m with 984 segments.

ELT primary mirrors are subject to various effects that can modify the relative position of the segments such as the variation of the gravity vector with respect to the telescope, thermal variations, wind, and vibrations. This is why the position of each segment must be actively measured and controlled in piston, tip, and tilt to reach optical performances of ~10 nm rms on the wavefront. The strategy currently foreseen is a combination of edge sensors to monitor the shape of the primary mirror in real-time and of an optical phasing sensor (OPS) to provide zero reference with nanometer precision for these sensors at regular intervals. Indeed, the accuracy of edge sensors is strongly affected by external conditions such as mechanical alignment, temperature, and humidity. An absolute reference is thus needed to recalibrate these sensors and keep low cophasing errors. Current OPS designs are based on Shack–Hartmann wavefront sensors similar in their
principle to the one used in the Keck telescopes [3,4], but several other concepts of sensors have been studied.

Requirements faced by these OPSs when cophasing a segmented mirror are of two kinds: (1) the coarse initial phasing of the mirror and (2) the very fine phasing at high precision. The latter is essential to reach the highest optical performances when constraints on the wavefront are exceptionally high, in particular, for applications such as direct detection of exoplanets with extreme adaptive optics and coronagraphy on an ELT [5-7], for which a precision of a few to 30 nm rms must be obtained to reach contrasts of $10^{-8}$ to $10^{-9}$. The former is equally important for the initial phasing of the primary mirror when segments will be installed for the first time on the telescope. It is also foreseen to be faced on a daily basis in the E-ELT for which 2 of the 984 segments will be replaced every day for recoating. Mechanical alignment of the segments will provide a cophasing precision of $\sim 20 \mu m$ on the wavefront, leaving the remaining correction down to $\sim 10 \text{nm rms}$ for a dedicated OPS.

It is in this context that the Active Phasing Experiment (APE) [8] was designed to test four concepts of OPS in the laboratory and on the Very Large Telescope (VLT). The four sensors are a Shack–Hartmann sensor [9], a pyramid sensor [10], a curvature sensor [11], and a Zernike phase contrast sensor [12]. The APE bench includes a small (153 mm in diameter) segmented mirror constituted of 61 segments controllable independently in piston, tip, and tilt [13], dimensioned to reproduce future ELTs in terms of segment size and gaps between segments when seen from the OPS. The VLT pupil is reimaged on the active segmented mirror (ASM) in order to create a fake 8 m segmented pupil which can be analyzed and corrected by the four sensors. Since the APE is installed on a Nasmyth platform and does not include a pupil derotator, the VLT pupil, and in particular the spiders, rotates with respect to the segmentation pattern created by the ASM. This can lead to phasing errors when the spiders are in a configuration that isolates different areas of the ASM by covering almost aligned segment borders. This problem is specific to APE and will not take place in a real ELT where the spider will remain fixed with respect to segmentation. The absolute position of each segment in the APE is referenced by an internal metrology (IM) system [14] that is used to control the ASM with a precision better than 5 nm rms several times per second. By means of the IM, the ASM can be set in any configuration of piston, tip, and tilt within the limits of $\pm 14.4 \mu m$ in piston on the wavefront, which is the measurement range of the IM.

One of the sensors in the APE is the Zernike phase contrast sensor, also called the ZErnike Unit for Segment phasing (ZEUS), was developed by the Laboratoire d’Astrophysique de Marseille in collaboration with the European Southern Observatory and the Instituto de Astrofísica de Canarias. The ZEUS finds its origins in the Mach–Zehnder (MZ) phasing sensor concept [15,16], replacing the delicate interferometer setup by a simple phase mask [12]. Similar to the Zernike phase contrast approach [17], it has been found equivalent to the MZ in terms of performance characteristics. The phase mask, located in the telescope focus, takes the form of a cylindrical depression machined into a glass substrate. Its diameter is close to that of the seeing disk, and its depth corresponds to a phase shift between $\pi/4$ and $\pi/2$ of the light transmitted through the mask compared to that transmitted through the surrounding substrate. Following the mask, a lens projects an image of the telescope pupil onto a detector array. When the observed star is centered on the mask, pupil aberrations appear as intensity variations on the detector as in the classical phase contrast method, but since the mask is larger than the diffraction spot, low-frequency aberrations, in particular those due to atmospheric turbulence, are filtered out. Piston errors between segments, containing important high-frequency components, show up as antisymmetric intensity variations along segment edges. Enlarging the mask diameter eliminates more of the atmospheric aberrations but reduces at the same time the width of the antisymmetric signal, making it more difficult to measure. A similar trade-off is also found for mask depth: a deep mask, giving a $\pi/2$ phase shift, provides a stronger signal than a shallower mask, but the signal also contains a larger symmetric component, which is found to reduce the accuracy of the signal fitting algorithm, particularly for large piston errors. To allow for different observing conditions, stellar magnitudes, observing wavelength, and initial phasing errors, five different phase masks are available in the ZEUS, with a depth of 100 or 175 nm, and a diameter of 1.0, 1.5, and 2.0 in. [18]. All the results reported here were obtained using the 175 nm thick masks.

Theoretical treatment of the ZEUS and fine cophasing performance within the single-wavelength capture range with the ZEUS has been studied in Surdej et al. [19] using observations performed on the APE bench at the VLT. Here, we present the results obtained during the same observing runs using a closed-loop multiwavelength phasing scheme, which allows reaching a capture range of several micrometers. We first describe our phasing scheme in Section 2. Then in Section 3, we present the two observing runs of February and April 2009 with the different configurations that have been tested. In Sections 4 and 5, we present the results obtained on-sky when phasing at a single wavelength in open- and closed-loop with large piston errors, respectively, and when using our multiwavelength scheme to estimate and correct these errors. In Section 6, we extrapolate our results to elaborate a phasing strategy for an actual ELT, and finally in Section 7, we briefly compare our results with a Shack–Hartmann-type sensor.
2. Multiwavelength Phasing Scheme

In this Section, we present a multiwavelength phasing scheme which allows reaching a capture range of several micrometers in piston. Before generalizing to a complete segmented mirror, we consider the ideal situation of two segments having one border in common that we wish to cophase. The two segments have absolute piston values of \( p_1 \) and \( p_2 \), respectively, generating a phase difference \( \Delta \phi = \frac{2 \pi}{\lambda}(p_2 - p_1) = \frac{2 \pi}{\lambda} \Delta p \) at their common border; \( \Delta p \) is called the edge piston. Unless specified otherwise, from now on, all values will be given in units of \( \lambda \) or in nanometers on the wavefront.

A. Capture Range in an Open Loop

The ZEUS normalized signal is constituted of two parts: an antisymmetric part, which is equivalent to the signal obtained with an MZ interferometer \[16\], and a symmetric part, which is specific to the ZEUS signal. The amplitude of the antisymmetric part is proportional to the sine of the phase difference between the two segments

\[
S_{\text{asym}} = A \sin(\Delta \phi),
\]

where \( A \) is a calibration coefficient, which depends on the phase mask physical properties (thickness and diameter) and the observing conditions (seeing). The phasing algorithm developed for the ZEUS allows to retrieve the value of \( S_{\text{asym}} \) through signal fitting \[19\], an thus to determine the value of \( \Delta p \) with

\[
\Delta p = \frac{\lambda}{2\pi} \Delta \phi = \frac{\lambda}{2\pi} \arcsin\left(\frac{S_{\text{asym}}}{A}\right).
\]

Since \( S_{\text{asym}} \) is a periodic function of \( \Delta \phi \), the range of measurable edge pistons is therefore limited to \( \pm \lambda / 4 \) on the wavefront when operating in an open loop. In the following Sections, we are going to see how this very narrow capture range can be extended by the use of a closed loop and several wavelengths.

As mentioned by Surdej et al., the symmetric part of the ZEUS signal \( S_{\text{sym}} \), which is proportional to \( \cos(\Delta \phi) \), could be used to extend the capture range to \( \pm \lambda / 2 \). However, on-sky results have shown that the value retrieved for \( S_{\text{sym}} \) through signal fitting is not reliable, and thus cannot be used to remove ambiguity on the edge piston estimation, limiting the effective capture range to \( \pm \lambda / 4 \). We note that the amplitude of the symmetric part strongly depends on mask thickness, so the use of a thinner phase mask gives a cleaner, more easily exploitable signal.

B. Closed Loop Phasing

Another possibility to extend the capture range to \( \pm \lambda / 2 \) is to perform closed-loop operation of the OPS. The main idea behind this concept is that for an edge piston \( \Delta p \in [\lambda / 4, \lambda / 2] \), the correction calculated assuming \( \Delta p \in [0, \lambda / 4] \) will necessarily be oriented toward a decrease of the edge piston. By performing successive measurements and corrections, the edge piston will eventually be brought into the open-loop capture range, and then to zero. This procedure is illustrated in Fig. 1, where an edge piston \( \Delta p_0 = 0.41 \lambda \) is first estimated to 0.09 \( \lambda \), leading to a new edge piston \( \Delta p_1 = (0.41 - 0.09) \lambda = 0.32 \lambda \) which is still in \( [\lambda / 4, \lambda / 2] \). The following estimation of 0.018 \( \lambda \) leads to a third edge piston \( \Delta p_2 = 0.14 \lambda \), which is now within \( [0, \lambda / 4] \), leading to a final correction that removes the remaining edge piston.

This closed-loop process can be applied for edge steps within \( [\lambda / 2, -\lambda / 2] \) but also around any multiple of \( \lambda \), i.e., in \( [\lambda(n - 1/2), \lambda(n + 1/2)] \), with \( n \) as an integer. In that case, the closed-loop process will bring the edge piston \( \Delta p \) toward \( n \lambda \).

C. Dual-Wavelength Phasing

If the edge piston \( \Delta p \) is larger than \( \lambda / 2 \), the single-wavelength capture range is not sufficient for phasing the two segments with a zero phase error but only to the closest integer multiple of \( \lambda \), leaving an ambiguity of \( n \lambda \). The only way to increase the capture range is to use multiple wavelengths to measure and remove this ambiguity. Two-wavelength interferometry, and in particular how to choose the right wavelengths, has already been extensively described in literature \[20\] with several improvements \[21, 22\]. However, these methods require accurate measurements at two distinct wavelengths. As will be shown in Subsection 4.A, the ZEUS measurement accuracy in an open-loop on-sky is rather poor, requiring the use of a different method. The multiwavelength scheme that was adopted for the ZEUS \[18\] uses closed-loop phasing at two separate wavelengths \( \lambda_0 \) and \( \lambda_1 \) \[23\], in order to determine and remove the ambiguity on the edge piston.

Phasing is first performed at \( \lambda_0 \), until convergence is reached. The edge piston is then \( \Delta p_0 = n \lambda_0 \), with \( n \) as an integer. The wavelength is switched to \( \lambda_1 \), so that a new edge piston \( \Delta p_1 = n \lambda_1 \) appears:
\[ \Delta \Pi = \Delta p_0 - \Delta p_1 = n\lambda_0 - n\lambda_1 = n\Delta \lambda, \]  
\[ \text{where } \Delta \lambda = \lambda_0 - \lambda_1. \text{ While } \Delta p_0 \text{ and } \Delta p_1 \text{ are unknown, we assume that the difference between them, } \Delta \Pi, \text{ is known. The ambiguity } n \text{ can then be easily determined from Eq. (3):} \]
\[ n = \frac{\Delta \Pi}{\Delta \lambda}. \]  
In order for the ambiguity \( n \) to remain identical for the two wavelengths, Eq. (4) is valid only as long as
\[ |\Delta \Pi| < \frac{\lambda}{2}, \]  
with \( \lambda = (\lambda_0 + \lambda_1)/2 \). With the approximation that \( \Delta p \approx n\lambda \), Eqs. (4) and (5) lead to the following condition of validity:
\[ 2|\Delta p| \lesssim \frac{\lambda^2}{\Delta \lambda}. \]  
For simplicity, we note \( \Lambda = \frac{\lambda^2}{\Delta \lambda} \) the synthetic wavelength, which is a function of only the two wavelengths \( \lambda_0 \) and \( \lambda_1 \). The new multiwavelength capture range in a closed loop is then equal to \( \pm \Lambda/2 \).

The multiwavelength phasing is illustrated in Fig. 2. In practice, \( \Delta \Pi \) is determined by performing phasing of the segments at \( \lambda_1 \) while recording the successive corrections that are applied on individual segments until convergence is reached at \( \lambda_1 \). Ambiguity is then determined with Eq. (4) for every segment and finally removed.

Contrary to other methods ([21,22]) which require to carefully choose the wavelengths, the choice here is mainly driven by the difference \( \Delta \lambda \), over which the capture range depends. Two close wavelengths will provide a wide capture range but will be less precise for small piston errors because the piston difference between the two phased positions will be small, and thus more sensitive to errors. On the contrary, more widely separated wavelengths will provide a shorter capture range, but a greater precision for small piston errors.

D. Generalization and Practical Implementation

The closed-loop and multiwavelength schemes from Subsections 2.B and 2.C have been illustrated in the case of two segments having one border in common. However, these schemes can be generalized to a complete segmented mirror with hexagonal geometry. As a matter of fact, the edge piston values at the borders of each segment are related to the segment piston of each segment by a system of linear equations. The segment piston defined with respect to a reference segment which has a piston \( p = 0 \) by definition. The determination of the edge piston at all segment borders then allows deducing the piston of each segment by the resolution of a set of linear equations using singular value decomposition (SVD).

Another important aspect, which has been overlooked in the previous Sections, is the measurement noise. In the presence of noise, the OPS will never see a completely phased mirror, i.e., the peak-to-valley (PtV) and rms values of the measured piston errors will never be zero. It is then necessary to define a convergence criterion, which tells if the mirror is phased from the point of view of the OPS. This criterion has been defined as thresholds \( T_{\text{PtV}} \) and \( T_{\text{rms}} \) on the PtV and rms values of the measured piston errors: for the mirror to be considered as phased, the PtV and rms must both be lower than their respective thresholds. Their exact value is not critical, they must simply be tight enough to phase the mirror with sufficient accuracy, but loose enough to prevent oscillating around the phased configuration because of measurement noise. The optimal values depend on several parameters such as observing conditions, wavelength, and phase mask properties. In practice, we used previous results obtained in similar conditions to choose appropriate values, which were in general around \( \sim 20 \text{ nm} \) for \( T_{\text{rms}} \) and \( \sim 50 \text{ nm} \) for \( T_{\text{PtV}} \). Further study and observations would be required to define an automatic adjustment procedure for these values.

The calibrations for the multiwavelength scheme leading to the normalized image are identical to that of the single-wavelength scheme [19]: a dark frame and a reference image taken without the phase mask. For the latter, it is sufficient to off center the mask by a few arcseconds to eliminate its influence on the signal at the segment edges. It is necessary to acquire such an image in each filter used for the multiwavelength scheme.

Fig. 2. Multiwavelength phasing scheme illustrated with \( \lambda_0 = 750 \text{ nm} \) and \( \lambda_1 = 650 \text{ nm} \). Phasing is first performed at \( \lambda_0 \) for the edge piston to converge to \( n\lambda_0 \), then the wavelength is switched to \( \lambda_1 \) and phasing is performed again until convergence. The \( \Delta \Pi \) piston difference between the two phased positions is directly related to the ambiguity \( n \) and the two wavelengths (see text for details).
3. Observations

The ZEUS was tested on-sky during a total of six nights from December 2008 to April 2009. A small part of two half-nights (~6 h in total) was dedicated to study multiwavelength phasing of large piston errors in February and April 2009, respectively. Different random configurations were applied on the ASM ranging from 600 to 8000 nm PtV on the wavefront, outside of the single-wavelength capture range of the ZEUS. All these observations were performed on bright stars with magnitudes comprised between $V = 4.0$ and $V = 5.0$ to avoid being in a noise-limited phasing regime. Investigations of performance in the photon starving regime have been presented by Surdej et al.

In February 2009, the 600, 1200, and 2000 nm PtV random configurations were tested with narrowband filters at $\lambda_0 = 750 \text{ nm}$ ($\Delta \lambda = 40 \text{ nm}$) and $\lambda_1 = 650 \text{ nm}$ ($\Delta \lambda = 40 \text{ nm}$), producing a multiwavelength capture range of $\pm 4.9 \mu \text{m}$. Observing conditions were average, with seeing varying between 0.7 and 1.2 in.. The diameter of the phase mask used for the observations was 1.5 in., and its thickness was 175 nm.

In April 2009, the 2000, 6000, 7000, and 8000 nm PtV random configurations were tested at $\lambda_0 = 800 \text{ nm}$ ($\Delta \lambda = 40 \text{ nm}$) and $\lambda_1 = 750 \text{ nm}$, producing a capture range of $\pm 12.0 \mu \text{m}$. Observing conditions were good, with a seeing disk around 0.7 in., leading to the use of a smaller mask of 1.0 in. with a thickness of 175 nm.

4. Single Wavelength Results

In this Section, we present the results obtained both in the open and closed loop at a single wavelength. We focus on the analysis of the results at the level of segment borders, where the normalized signal is measured and converted into an edge piston.

A. Open-Loop Performance

The ZEUS shows poor open-loop performance mainly due to large fitting errors in the determination of $S_{\text{asym}}$. Although the ZEUS capture range is intrinsically limited to $\pm \lambda/4$ when fitting only the antisymmetric part of the signal, it is interesting to evaluate the precision with which the signal is fitted in the open loop since it will impact on the convergence speed in the closed loop. Figure 3 shows a typical example for a 2000 nm PtV configuration of the ASM at $\lambda_0 = 750 \text{ nm}$. Iteration 0 represents the open-loop measurement on this configuration. The data points clearly follow a sinusoidal calibration curve, as expected from Eq. (1), but for edge pistons outside of $\pm \lambda/6$, the error can be as high as 50%. Within this range, the antisymmetric part $S_{\text{asym}}$ dominates, providing good accuracy on the signal fitting, while outside this range, the symmetric part $S_{\text{sym}}$ becomes more important, and the signal fitting is less accurate.

The loss of open-loop accuracy for edge pistons outside of the quasilinear part of the sine calibration curve is illustrated on Fig. 4, which shows the standard deviation of the error on the determination of $S_{\text{asym}}$ in bins of $\lambda_0/8$ for the same ASM configuration and iterations as Fig. 3. At iteration 0, all bins are populated with 15 to 20 points (ensuring reliable statistics), and we see that the fitting error clearly increases for edge pistons outside of $\pm \lambda/8$, thus providing accurate measurements only close to zero. This poor open-loop performance, even within the single-wavelength capture range, requires the use of closed-loop phasing to bring all edge pistons close to zero.

B. Closed-Loop Performance

Although open-loop performance is poor, all edge pistons finally converge toward integer multiples of $\lambda_0$ in the closed loop. Surdej et al. have shown that convergence is reached with good accuracy for edge

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![Fig. 3. (Color online) ZEUS antisymmetric part of the signal, $S_{\text{asym}}$, as a function of the edge piston on the wavefront given by the IM, (a) and the same measurements folded within $\pm \lambda_0/2$, (b) for the 2000 nm PtV random configuration on the ASM at $\lambda_0 = 750 \text{ nm}$. Measurements are given for three iterations during closed-loop phasing. Iteration 0 corresponds to the initial unphased configuration. The ASM is partially phased at iteration 5, and completely phased at iteration 10 according to the ZEUS. Borders covered by the VLT pupil and spiders have been removed (see text for details).](2712 APL OPTICS 50 17/10 June 2011)
pistons within a single-wavelength capture range, but we now demonstrate that the same result is obtained for edge pistons around larger integer multiples of \( \lambda_0 \). We see in Fig. 3 that all edge pistons are within \( \pm \lambda_0/4 \) around a multiple of \( \lambda_0 \) after five iterations, and within \( \pm \lambda_0/10 \) after 10 iterations, when the ASM is considered to be phased for the ZEUS.

In Fig. 4, we see that although the error is large and far from zero, all edge pistons finally converge in the closed loop after 10 iterations because the small error in the linear part of the calibration curve allows to retain edge pistons in that area once they are close enough to the zero phase error. The same behavior is observed for all other configurations tested on-sky: at the last iteration in single wavelength, most edge pistons are within \( \pm \lambda_0/10 \) around a multiple of \( \lambda_0 \), and the error on \( S_{\text{asy}} \) is below 0.2. In the next Section, we will see how this result translates into the determination of the piston error of the segments.

5. Multiwavelength Results

As we have seen from the previous Section, edge pistons converge in a closed loop toward an integer multiple of the wavelength. In this Section, we are going to see how it leads to the phasing of the ASM at independent wavelengths and how it allows the determination of the piston ambiguity for each segment. From now on, we will analyze the results at the level of the segments, i.e., after solving the linear system of equations with SVD that converts the edge pistons into estimated segment piston errors with respect to an arbitrary zero position. These estimates are fed back to the ASM, leading, eventually, to convergence to a phased state, at least in a single-wavelength sense. The absolute piston of the segments is measured by the IM, allowing us to follow the phasing process iteration by iteration and to see the exact position of each individual segment.

A. Convergence at Two Wavelengths

The convergence of all edge pistons toward integer multiples of \( \lambda \) can equivalently be seen as the convergence of the piston error of each segment toward an integer multiple of \( \lambda \). This process is illustrated in Fig. 5, which shows the piston error of each segments of the ASM for the 24 iterations that have been performed for the configuration previously shown. This allows us to follow the evolution of individual segments or groups of segments. For all ASM configurations that were tested on-sky, the following progression is observed.

1. Convergence at \( \lambda_0 \) from a totally random configuration is somewhat chaotic; segments with similar piston errors at the first iteration can follow very different paths (e.g., segments 7 and 48 in Fig. 5).

2. After a certain number of iterations (the exact number depends on observing conditions and thresholds \( T_{\text{PIV}} \) and \( T_{\text{rms}} \)) convergence is reached at \( \lambda_0 \), and the wavelength is switched to \( \lambda_1 \).

3. The loop is closed at \( \lambda_1 \) until convergence is reached again. This process takes much less iterations since the mirror is already in an ordered state. Usually all segments converging at \( \lambda_0 \) will similarly converge at \( \lambda_1 \).

Convergence was reached for most segments in all ASM configurations tested on-sky, at the exception of a few cases that will be detailed in Subsection 5.D. Table 1 summarizes all the important phasing information in the closed loop at \( \lambda_0 \) and \( \lambda_1 \). In particular, we see that 10 to 30 iterations are necessary to reach phasing at \( \lambda_0 \), while only 4 to 11 iterations are necessary at \( \lambda_1 \). In most cases, all segments converge at
both wavelengths within $\lambda/6$ or better toward an integer of $\lambda_i$ translating into 10 to 30 nm rms phasing precision on the whole mirror. The final phasing performance is strongly related to the observing conditions, and in particular to the stability of the seeing, but these numbers are comparable to the results obtained in the closed loop around zero [19]. A larger sample of measurements would be necessary to draw final conclusions on the influence of seeing variations.

B. Ambiguity Determination

We now demonstrate that the accurate closed-loop convergence at both $\lambda_0$ and $\lambda_1$ allows us to determine and remove the $n\lambda$ ambiguity on the piston error of the segments to bring them within the single-wavelength capture range. The ambiguity is determined using Eq. (4) and then removed for each segment. The determination is considered successful for a segment if its piston error is within the single-wavelength capture range around zero after the ambiguity has been removed. The results obtained on-sky are presented in Fig. 6, which shows the proportion of segments within a single-wavelength capture range around zero, $\pm\lambda_0/2$, and larger multiples of $\pm\lambda_0$ (including segments outside of the multiwavelength capture range).

The essential result is that for six of the seven ASM configurations tested on-sky, 100% of the segments are in $[-3\lambda/2...3\lambda/2]$ after ambiguity removal, and at least 80% of them are in $[-\lambda/2...\lambda/2]$, which is the single-wavelength capture range. For the 8000 nm PtV configurations, two segments are completely lost because ambiguity determination was faulty, and two segments are within capture range around multiples of $\pm\lambda_0$ larger than 2. Using the multiwavelength scheme again can of course allow to capture these last two segments.

The proportion of segments inside the single-wavelength capture range after ambiguity has removed decreases for configurations with large initial piston errors, at the benefit of segments that end up close to $\pm\lambda_0$. This is expected since the determination of the ambiguity is quite prone to small errors: the value determined from Eq. (4) is rounded to the closest integer, so small convergence errors at either $\lambda_0$ or $\lambda_1$ can potentially propagate to produce an error of $\pm 1$ on $n$. However, only large convergence errors or segments that did not converge at all could produce errors larger than 1.

Finally, we expect from these results that the number of lost segments will increase for configurations with larger PtV. In particular, configurations with large piston errors are more sensitive to convergence problems that can result in the loss of segments. Configurations having segments close to $\pm\Lambda/2$ or close to the coherence length of the filters will certainly end up with a large proportion of segments either with a very large piston error or within capture range of large multiples of $\lambda_0$. The way to overcome this limitation is to use filters with central wavelengths closer together that will offer a much larger capture range. However, this leads to larger uncertainty in the determination of the ambiguity $n$ (Eq. (4)), hence the piston error determination. A second couple of filters with wavelengths more widely separated would then be necessary to recover full phasing precision once all segments are within a few $\lambda$ around the zero position.

C. Systematic Effects

In these results, a systematic effect has been removed from the data to provide accurate values. On the ASM, the central segment cannot be actively controlled and is maintained in a fixed position to serve as the zero reference for measuring the piston error of all other segments. While this reference is usable by the OPS in a laboratory where there is no telescope pupil covering the ASM, it becomes useless
on the VLT where the central reference segment remains hidden behind the secondary mirror.

However, the IM always sees this reference segment and can thus provide a piston error measurement with respect to the central segment. This has no impact on edge piston measurements at all borders, which gives a relative positioning information between segments. But when converting the edge piston information into piston error measurements through SVD, the lack of absolute reference introduces a variable offset in all segment piston determined by the OPS. This changing reference can be referred to as a “floating” reference.

This effect is just an artifact introduced by the IM, and it has no impact on the final single-wavelength phasing performance or on the $n\lambda$ ambiguity determination: the ZEUS phases all segments together, simply ignoring the central one, which is the reference for the IM. This is why the floating reference has been estimated and removed from the data presented in Fig. 5 and Table 1. The estimation is performed at the last iteration of each wavelength using the segments phasing close to zero (zero being defined by the IM). The systematic offset of this group of segments has been measured and removed from all previous iterations at the same wavelength.

D. Convergence Problems

Although in most cases all segments converge toward an integer multiple of $\lambda_0$ or $\lambda_1$, there are two notable exceptions visible in Table 1: the 600 nm PtV configuration at both wavelengths, and the 8000 nm PtV configuration at $\lambda_0$, for which a few segments failed to converge. These segments have been highlighted in Fig. 7 on the science images obtained for the last iteration at $\lambda_0$. This failure mainly affects segments which are partly covered by the telescope pupil, and where the number of usable borders is generally limited to two or three instead of six, leaving a possible ambiguity on the determination of the piston error of the segment. The spiders can also cover some of the borders and distort the edge piston measurement. Moreover, adjacent segments are influenced by the misbehavior of their neighbor, resulting in groups of segments that fail to converge within the $\pm\lambda/6$ interval.

For the 600 nm PtV configuration [Fig. 7(a)], segments 48 and 58 remained stuck close to $-\lambda_0/4$, while segment 47 was influenced by segment 48 and converged only within $\pm\lambda_0/5$ around an integer multiple of $\lambda_0$. For the 8000 nm PtV configuration [Fig. 7(b)], a group of four adjacent segments failed to converge at $\lambda_0$: two of them are covered by the pupil and have only three borders available for analysis, and the spider is very close to one of these borders. These segments are highlighted in Fig. 8, and we can see that segments 34, 56, and 58 remained in between two integer multiples of $\lambda_0$, while segment 33 converged close to $-4\lambda_0$. Segment 54 is different, as it started to diverge at the very first iteration. However, it is interesting to see that all these segments finally converged after the wavelength was switched to $\lambda_1$. We can assume that starting from a partially phased ASM and using another wavelength, the uncertainties remaining for these segments were cleared, allowing a final convergence.

The main problem with these misbehaving segments comes when the $n\lambda$ ambiguity is determined and removed. Since they did not converge properly at one or both of the wavelengths, their value of $n$ can potentially be wrong, sending them outside of the multiwavelength capture range. This is exactly what happened for segments 54 and 58 in the 8000 nm PtV configuration: the sign of $\Delta\Pi$, and thus of $n$, was erroneous, and they were sent outside of $\pm\Lambda/2$. For the 600 nm PtV configuration, since the piston errors are already close to zero, the error on $n$ cannot be larger than 1, which explains why in the end all segments are still within $\pm3\lambda/2$.

E. Summary and Limitations

In the previous Sections, we have presented various results for the multiwavelength scheme of the ZEUS.

For clarity, different information have been summar-
ized in Table 2. They are divided in three categories: the starting configuration, the state after the ambiguity has been determined and removed, and the state when the phasing procedure was ended. The phasing procedure was generally stopped before reaching a new phased state, so the final PtV and rms values are not necessarily reflecting the ultimate result, but it gives a general view of the number of phased, recoverable, and lost segments.

With the use of the multwavelength scheme, the piston error of most segments is largely reduced, as can be seen for example in Fig. 8. The initial coarse phasing would then be followed by another application of the scheme for a finer phasing with a second pair of wavelengths offering a less extended capture range. Some of the segments have been either lost (only two in the configuration with largest piston errors) or did not converge properly. The latter are, however, recoverable since their piston error still lies within the multwavelength capture range.

There are two main limitations inherent to the APE system limiting the performance of the ZEUS. The first is that there is no pupil derotator, which means that the spiders are rotating with respect to the segmentation pattern, creating a difference between the images being analyzed and the calibration images taken at the beginning of the phasing procedure. The second is the convergence problems of some segments described in Subsection 5.D. It mostly concern segments covered by the telescope pupil edge (or their close neighbors) for which the linear system between the edge pistons and the segment piston error is less overdetermined. To better represent a real segmented telescope, the ASM should have been smaller than the VLT pupil.

6. Phasing Strategy for an ELT

These results can now be analyzed in terms of phasing strategy for a future ELT. We have seen from previous Sections that the phasing of large piston errors with our multwavelength scheme is reliable up to 7000 nm PtV, and that it could certainly be made more reliable for even larger piston values using filters closer together in wavelength. With a couple of filters at 750 and 725 nm, the capture range would be ±Λ/2 = ±10.9 μm. This capture range would be sufficient to phase an ELT primary mirror, which has been mechanically phased with a precision of ~20 μm, or to recapture a segment that has been changed and reinstalled with equivalent precision.

For an actual ELT, a three-step phasing strategy would appear optimal with a ZEUS-like sensor. First, coarse phasing using a very large capture range in order to remove the largest piston errors should be implemented using filters with wavelengths close together (e.g., 750 and 725 nm). Since a correspondingly small bandwidth, typically 10 nm, would be necessary to offer sufficiently long coherence length (~50 μm), a bright star (V ≤ 4) would be required for this step. A second step, using more widely spaced wavelengths (e.g., 750 and 650 nm) would bring all segments within the single-wavelength capture range. While correspondingly larger filter bandwidths can be used, a bright star would still be required to limit exposure time. Final phasing is now done using the single-wavelength regime. Here, a wide-band filter can be used, allowing the use of much fainter stars (V ≤ 10).

Considering the results presented here and by Surdej et al., phasing of an ELT would require a total of 80 to 100 closed-loop iterations depending on observing conditions in the case of a completely unphased primary mirror. Considering 10 to 20 s exposures, this would require between 15 and 35 min of exposure time. Including target acquisition (~10 min), calibrations (~5 min), and computing time (~20 s/iteration), this leads to a final estimate of less than 1 h 30 min for initial phasing of an ELT. For an already partially phased mirror, only the third step would probably be necessary, consequently reducing the amount of phasing time. Phasing of a single segment with respect to fixed neighbors was not studied, but we believe convergence would be much faster in this case.

Finally, it is important to underline the potential problem of the spiders. In APEs, the absence of a
pupil derotator makes the spider move with respect to the segmentation pattern, sometimes covering several segment borders. The worst configuration occurs when the spiders are almost aligned with borders, thus isolating different parts of the mirror from the point of view of the OPS. The upper right spider of Fig. 7(a) would be in such a configuration if it was rotated ∼5° clockwise. Inversely, the best configuration occurs when the spiders are almost orthogonal to segment borders similarly to the lower left spider of Fig. 7(b). Although it will still prevent good edge piston measurement for these borders, the parts of the mirror lying on each side of the spider will not be isolated from one another because the segments covered have borders on each side of the spider. In order to avoid potential phasing problems, the design of an ELT needs to take into account the size and position of the spiders to avoid as much as possible configurations where different parts of the mirror are isolated.

7. Comparison with a Shack–Hartmann Sensor

In this Section, we briefly compare the ZEUS with a Shack–Hartmann-type sensors. We base this discussion on the results published by Chanan et al. [3,4] on the phasing at the Keck telescopes with their “broadband algorithm”.

Contrary to a Shack–Hartmann-type sensor, the ZEUS does not require any particular alignment between the sensor and the telescope pupil. It is, therefore, mostly insensitive to alignment variations or optical distortion. Although the success of the Keck phasing sensor proves that such effects are perfectly manageable on a 10 m class telescope, they can be expected to have a larger impact on the phasing performance for larger telescopes. Also, if continuous phasing is implemented, requiring the use of a guide star whose position in the field varies, pupil distortion may not be constant during the observations. The only constraint for the ZEUS is the alignment of the phase mask in the focal plane of the telescope, which needs to be better than 0.1 in. on-sky (between 5% and 10% of the phase mask diameter). Such an alignment could be easily reached with the use of a tip–tilt corrector.

It has been shown that the ZEUS phasing accuracy is better than 10 nm rms with stars brighter than $V \approx 5$ [19], which is similar to the accuracy obtained at Keck with the narrow-band phasing algorithm [4]. When it comes to phasing using a faint star, the ZEUS has been shown to reach a precision of 15 nm rms for stars of magnitude $V \approx 13$. To the best of our knowledge, measurements in similar conditions have not been reported for any other sensor, but this is a criterion for comparison that could potentially be discriminating. Although the ability to phase with faint stars is not necessary for reducing large piston errors, it is certainly important if a continuous phasing strategy is foreseen. For the phasing of large piston errors, it seems that the ZEUS is very similar to the Keck Shack–Hartmann sensor in terms of performance and time required for phasing. Chanan et al. report reducing 30 μm errors in approximately 2 h. As explained in Section 6, such errors could be reduced with the ZEUS in less than 1 h 30 min (including calibration) using our multiwavelength scheme.

8. Conclusions

Cophasing of segmented primary mirrors is required to reach high wavefront quality of future ELTs. Given the large number of segments, it is necessary to be able to phase segments with piston errors of several micrometers and to reach a phasing precision of a few nanometers. Moreover, this phasing must be executed simultaneously for all segments. In this work, we have demonstrated on-sky the use of the Zernike phase contrast sensor for phasing of large piston errors using a multiwavelength scheme. Performing closed-loop phasing at two close wavelengths, it is possible to determine and remove the $n \lambda$ ambiguity on the piston of each segments.

Although the open-loop performance is poor due to large errors in the signal fitting procedure outside of $\lambda/4$ around each integer multiples of $\lambda$, the good precision of the fitting close to zero, where the antisymmetric part of the signal dominates, allows us to reach convergence in the closed loop after 10 to 30 iterations at the first wavelength, and in 3 to 11 at the second wavelength. In most cases, all segments phase within $\pm \lambda/6$ around an integer multiple of $\lambda$, so that the $n \lambda$ ambiguity can be estimated accurately. We have demonstrated that for all the ASM configurations tested on-sky, at least 90% of the segments are within $\pm 3 \lambda/2$ after ambiguity estimation, and for all configurations except the one with the largest PtV, 80% of the segments are inside $\pm \lambda/2$, i.e., inside the single-wavelength capture range around zero. Problems directly related to the APE experiment, such as the lack of a derotator, are identified as possible reasons for segments failing to converge properly.

We have also proposed a phasing strategy for an ELT with a ZEUS-like sensor. Using different couples of filters, very large piston errors could eventually be reduced in less than 1 h 30 min. We have also underlined important problems related to the spider position with respect to the segmentation pattern, and we advocate a configuration where the spiders are perpendicular to segment borders. Such a configuration would avoid isolating different parts of the mirror, resulting in independently phased areas. Finally, we conclude that the ZEUS offers similar performances to a Shack–Hartmann-type sensor, but it certainly is much more robust in the sense that it does not require any particular alignment with the pupil of the telescope. While this is not problematic in the case of a 10 m telescope, this would certainly be a clear advantage in the 30 to 42 m pupil.

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